

The above op-amp is ideal

$\therefore I_i = 0$ I_i - input current to Op-Amp

$V_{ii} = V_{2i}$ V_i, V_2 - the two $1/p$ voltage to Op-Amp

(a) Find $\frac{V_o(\omega)}{V_i(\omega)} = H(\omega)$ V_1 - Voltage at Node 1

To find relationship b/w $V_i(t)$ & $V_o(t)$ apply KCL at node 1

$$V_{2i}(t) = V_{1i}(t) = V_o(t).$$

$$\frac{V_1(t) - V_i(t)}{1K} + \frac{V_1(t) - V_o(t)}{1K} + 70n \frac{d(V_1(t) - V_o(t))}{dt} = 0$$

$$\frac{2V_1(t) - V_i(t) - V_o(t)}{1K} + \frac{70}{10^9} \frac{d}{dt} (V_1(t) - V_o(t)) = 0.$$

$$V_1(t) \left(2 + 70 \times 10^{-6} \frac{d}{dt} \right) - V_o(t) \left(1 + 70 \times 10^{-6} \frac{d}{dt} \right) - V_i(t) = 0$$

~~REARRANGE~~

~~REARRANGE~~

~~REARRANGE~~

Take FT

$$V_1(\omega) \left(2 + j\omega 70 \times 10^{-6} \right) - V_o(\omega) \left(1 + j\omega 70 \times 10^{-6} \right) - V_i(\omega) = 0 \quad \text{--- (1)}$$

Take KCL at V_1

②

$$\frac{V_o(t) - V_1(t)}{1K} + 35n \frac{dV_o(t)}{dt} = 0.$$

$$V_o(t) - V_1(t) + 35 \times 10^{-6} \frac{d}{dt} V_o(t) = 0$$

TAK FT.

$$V_o(\omega) - V_1(\omega) + V_o(\omega)j\omega (35 \times 10^{-6}) = 0$$

$$V_1 = V_o(1 + j\omega (35 \times 10^{-6})) \quad \text{--- } ②$$

Plug ② in ①.

$$V_o(1 + j\omega (35 \times 10^{-6})) (2 + j\omega \underline{70 \times 10^{-6}}) - (1 + j\omega \underline{70 \times 10^{-6}}) V_o = V_{in}$$

$$\frac{V_o}{V_i} = H(\omega) = \frac{1}{(2 + j\omega \underline{70 \times 10^{-6}} + j\omega \underline{70 \times 10^{-6}} - 2\omega^2 (35 \times 10^{-6})^2) - 1 - j\omega \underline{70 \times 10^{-6}}}$$

$$= \frac{1}{1 + j\omega \underline{70 \times 10^{-6}} - 2(\omega^2 35 \times 10^{-6})^2}$$

it would
have been
more clear
if $1K = R$.
 $75nF = C_1$,
 $35nF = C_2$

The underline 70×10^{-6} is in fact

$$2 C_2 = 70 \times 10^{-6} \text{ if } \omega.$$

had not cancelled $1K$. The resulting expression would have been in terms of RC .

which would help in part (b).

(3)

(b)

As given in the book.

The -3dB bandwidth/freq is when

$$\frac{P_o}{P_i} = \frac{1}{2}$$

Take that in dB scale.

$$10 \lg \left[\frac{P_o}{P_i} \right] = 10 \lg \left(\frac{1}{2} \right) = -3 \text{dB}.$$

The freq at this point is called corner freq ' w_c '. For this 2nd order Butterworth

$$w_c = \frac{1}{\sqrt{2} R C_2} \approx 20200 \text{ rad/sec.}$$

(2)
(9)

(4)

Acc. to Shannon's Sampling theorem to avoid aliasing

$$w_s \geq 2w_m$$

where w_s - Sampling freq.

w_m - highest Freq Comp. of signal

As we multiply $x(t)$ with an impulse train,
clearly we are sampling $x(t) \rightarrow x_p(t)$ and then
reconstruct it as $y(t)$

$$w_s \geq 2w_m$$

$$\frac{2\pi}{T} \geq 2w_m$$

$$T \leq \frac{\pi}{w_m}$$

(b) For $y(t) = x(t) x_p(t)$ must pass through
1 low pass with filter ~~and~~

$$H(\omega) = T \operatorname{rect}(\omega/w_s)$$

(C)

For $T=0.004 \text{ sec.}$

$$\omega_s = \frac{2\pi}{T_s} = \frac{2\pi}{0.004} = 500\pi$$

$$\boxed{\begin{aligned} f &< 700 \text{ Hz} \\ \omega &< 1400\pi \end{aligned}}$$

(5)

$$x(t) = \cos(200\pi t)$$

$$p(t) = \sum_{K=-\infty}^{\infty} \delta(t - KT)$$

$$x_p(t) = x(t) * p(t).$$

$$X(\omega) = \pi (\delta(\omega - 200\pi) + \delta(\omega + 200\pi))$$

$$P(\omega) = \omega_s \sum_{k=-\infty}^{\infty} \delta(\omega - k\omega_s)$$

$$x_p(\omega) = F[x(t) * p(t)]$$

$$= \frac{1}{2\pi} X(\omega) * P(\omega)$$

$$= \frac{\omega_s}{2\pi} \left(\sum_{k=-\infty}^{\infty} [\pi(\delta(\omega - 200\pi) + \delta(\omega + 200\pi))] * \delta(\omega - k\omega_s) \right)$$

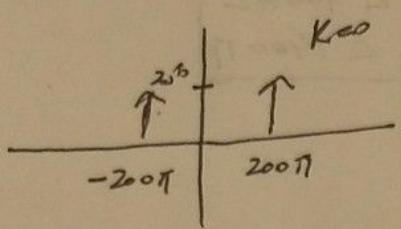
$$= \frac{\omega_s}{2} \sum_{k=-\infty}^{\infty} [\delta(\omega - 200\pi - \omega_s k) + \delta(\omega + 200\pi - \omega_s k)]$$

$$\text{As, } \omega_s = 500\pi$$

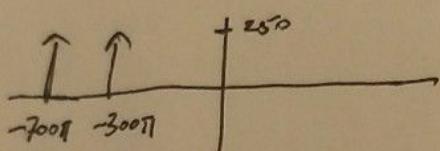
$$x_p(\omega) = 250 \sum_{k=-\infty}^{\infty} [\delta(\omega - 200\pi - 500\pi k) + \delta(\omega + 200\pi - 500\pi k)]$$

Plot for $K=0, \pm 1, \pm 2$ — for $\omega < 1400\pi$

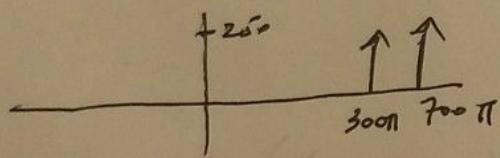
(6)



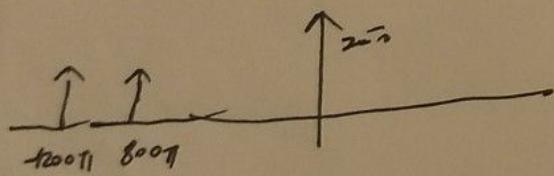
$K=1$



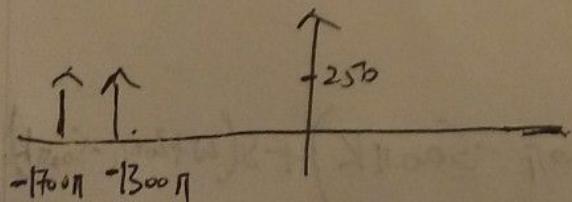
$K=-1$



$K=+2$



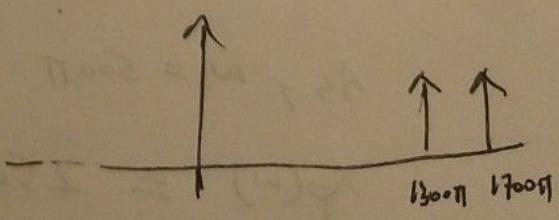
$K=+3$



freq Components below 1400π are.

$\pm 200\pi, \pm 300\pi, \pm 700\pi, \pm 800\pi,$
 $\pm 1200\pi, \pm 1300\pi.$

$K=-3$



$$(d) x(t) = \cos(2\pi f_n t)$$

(7)

$$\text{In part c } f_s = 100 \text{ Hz} \quad \omega = 200\pi$$
$$\omega_s = 500\pi$$

We need to find ω such that it has the same frequencies

- ① Notice the lowest freq comp $\pm 200\pi = \mp (500\pi(1) - 300\pi)$ For $K=1$
- ② similarly the sec. freq comp $\pm 300\pi = \mp (500\pi(0) - 300\pi)$ For $K=0$

This is only possible for $\omega = 300\pi$

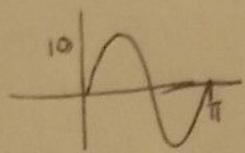
$$x(t) = \cos(300\pi t)$$

Notice $K \neq 2 \neq 3$ you will get the other components.

(3)

⑧

(a)

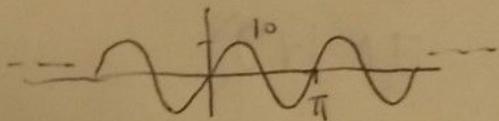


The above wave form is an ideal sine wave that exists for only one cycle. With Amp = 10 & Period = π sec with $t = 0$. $\omega = 2\pi f$ $f = \frac{1}{\pi}$

$$\boxed{\omega = 2}$$

~~ABNORMAL~~ with above parameters
Normal sine wave, from $-\infty$ to ∞

$$10 \sin(2t)$$



To limit sine wave from $0 - \pi$ we use the concept of unit step function.

$$v(t) \rightarrow \begin{cases} 1 & t \geq 0 \\ 0 & t < 0 \end{cases}$$

$$v(t-\pi) \rightarrow \begin{cases} 1 & t \geq \pi \\ 0 & t < \pi \end{cases}$$

$$[v(t) - v(t-\pi)] \rightarrow \begin{cases} 1 & 0 \leq t < \pi \\ 0 & \text{elsewhere} \end{cases}$$

This is one in our area of interest & 0 everywhere else.

$$\therefore \boxed{f(t) = 10 \sin(2t) [v(t) - v(t-\pi)]}$$

$$(b) L[f(t)] = F(s) \quad (9)$$

$$F(s) = \int_{-\infty}^{\infty} f(t) e^{-st} dt$$

$$= \int_{-\infty}^{\infty} 10 \sin(2t) [v(t) - v(t-\pi)] e^{-st} dt$$

~~If we change the integral limits from 0 - π~~
we can express the above expression as :

$$F(s) = \int_0^{\pi} 10 \sin(2t) e^{-st} dt$$

From Integration table .

$$\int e^{xt} \sin(yt) dt = \frac{1}{x^2 + y^2} [e^{xt} (x \sin(yt) - y \cos(yt))] + C$$

$$\therefore F(s) = \frac{10}{s^2 + 4} [e^{-st} (-s \sin(2t) - 2 \cos(2t))] \Big|_0^{\pi}$$

$$= \frac{10}{s^2 + 4} \left[\left[e^{-s\pi} (-s(0) - 2(1)) \right] - \left[e^{-s(0)} (-s(0) - 2(1)) \right] \right]$$

$$= \frac{10}{s^2 + 4} (-2e^{-s\pi} + 2)$$

$$= \frac{20}{s^2 + 4} (1 - e^{-s\pi})$$

$$(C) f(t) = 10 \sin(2t) [u(t) - u(t-\pi)] \quad (10)$$

$$f(t) = 10 \sin(2t) (u(t)) - 10 \sin(2(t-\pi)) u(t-\pi)$$

$$\mathcal{L}[f(t)] = F(s)$$

$$F(s) = \mathcal{L} [10 \sin(2t) (u(t))] - \mathcal{L} [10 \sin 2(t-\pi) u(t-\pi)]$$

$$= 10 \int_{-\infty}^{\infty} \sin 2t u(t) dt - 10 \int_{-\infty}^{\infty} \sin 2(t-\pi) u(t-\pi) dt$$

$$= 10 \int_0^{\infty} \sin 2t dt - 10 \int_0^{\infty} \sin 2(t-\pi) u(t-\pi) dt$$

From table 7.2 Property 10: $\boxed{\mathcal{L}[\sin(bt)] = \frac{b}{s^2 + b^2}} \quad (1)$

From Eq 7.21 (Real shifting) to 7.22

$$\begin{aligned} \mathcal{L}[f(t-t_0) u(t-t_0)] &= \int_0^{\infty} f(\tau) e^{-s(\tau+t_0)} d\tau \quad \text{where } \tau = t-t_0 \\ &= e^{-t_0 s} \int_0^{\infty} f(\tau) e^{-s\tau} d\tau \end{aligned}$$

$$\therefore \boxed{\mathcal{L}[f(t-t_0) u(t-t_0)] = e^{-t_0 s} F(s)} \quad (2)$$

using (1) & (2)

$$\Rightarrow F(s) = 10 \left[\frac{2}{s^2 + 4} \right] - 10 e^{-\pi s} \frac{(2)}{s^2 + 4}$$

$$= 20 \left(\frac{1 - e^{-\pi s}}{s^2 + 4} \right)$$